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July 27, 1960

COMPARISON OF WIND INPUT DATA FOR USE IN DETERMINATION OF MISSILE AND SPACE VEHICLE DESIGN BY STATISTICAL METHODS

by Joseph William Haughey William W. Vaughan

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> by Joseph William Haughey William W. Vaughan

DYNAMICS ANALYSIS BRANCH
AEROPHYSICS AND GEOPHYSICS BRANCH
AEROBALLISTICS DIVISION

ABSTRACT

This report presents a comparison of selected statistical wind summaries compiled from upper air observations made at Patrick AFB, Florida. A description of how this data was developed into convariance matrices is presented. Also a brief outline of how these convariance matrices can be utilized in control and trajectory studies is considered.

ACKNOWLEDGMENT

The authors of this report gratefully acknowledge the assistance of Mr. D. H. Boen in the many computations required in a report of this type. The assistance of Mr. Sieja in developing a program for calculating the convariance matrices on the Burroughs 205 Computer is also acknowledged.

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I. INTRODUCTION

The ultimate objective in designing a missile or space vehicle would be to consider the simultaneous effects of its entire flight environment. This flight environment is composed of pressure, temperature, density, and winds usually random in nature, which may be described in a statistical form. The process for describing this environment should be nonstationary rather than the standard stationary method. Stationary random processes are characterized by a set of probability functions that are invariant with a change in the time origin. When variations with time take place, the process is said to be non-stationary. Since the missile or space vehicle changes altitude as a function of time, the wind velocity for any time varies as a function of both altitude and time. Therefore, non-stationary random processes should be used to properly describe the environment.

Previous efforts have considered the effects of wind velocities separately from wind gusts or turbulence. R. E. Bieber (see reference one) proposed a method which utilized non-stationary statistical methods to determine missile structural loads. He demonstrated how the effects of wind velocity combined with turbulence or gusts might be studied simultaneously. The purpose of this report is to compare the data that Mr. Bieber utilized for a one dimensional input with the data supplied by the Aerophysics and Geophysics Branch. This branch is preparing the required cross-correlation coefficients in order to complete the two dimensional wind input data. Work is also underway preparing the means, standard deviations, and correlation coefficients for atmospheric density at various geographical locations.

II. DEVELOPMENT OF THE COVARIANCE MATRIX FROM THE CORRELATION COEFFICIENTS AND STANDARD DEVIATIONS

The Geophysics and Aerophysics Branch of the Aeroballistics Laboratory supplied the data shown in Tables 2 and 3. The procedure followed in developing the wind covariance matrix is shown in Figure 1. The standard deviation at one altitude for the North-South (meridional) wind is multiplied by the standard deviation at another altitude and this product is then multiplied by the correlation coefficient relating these different North-South winds. This computation is repeated until all the values of the North-South covariance matrix are obtained. The same procedure is then repeated for the East-West zonal winds covariance matrix.

The North-South wind covariance is then added to the East-West wind covariance to form a combined matrix. To the diagonal terms of this combined matrix is added the diagonal terms of the North-South to the East-West covariance matrix and the diagonal terms of East-West to the North-South covariance matrix. The resultant matrix represents an incomplete two dimensional matrix. This matrix was utilized as a one dimensional input by Mr. R. E. Bieber (reference one). The resulting incomplete two dimensional matrix is symmetrical, consequently only a triangular matrix need be shown. The two dimensional matrix can be completely developed by utilizing the non-diagonal parts of the North-South with East-West and the East-West with the North-South covariance matrices.

III. DESCRIPTION AND COMPARISON OF THE COVARIANCE MATRICES PRESENTED IN THIS REPORT

The statistical procedures employed to develop the covariance matrices shown in Tables 4, 5, and 6 were identical. The basic data used to develop the covariance matrices were obtained from the correlation matrices shown in Tables 1, 2, and 3. The conversion of the correlation coefficients, and the standard deviations to the covariance matrices was accomplished by utilizing the following formula. (Where X and Y are random variables)

The main purpose of this report is to compare Mr. Bieber's covariances with those developed by the Aeroballistics Laboratory. Although the same procedures were employed in the computation of these matrices (Tables 4, 5, and 6), there exists differences in the results obtained. Tables 7, 8, 9, and 10 provides a comparison of Bieber's date with the Aeroballistics Laboratory Data. The values shown in Table 2 were subtracted from the values shown in Table 1, to form Table 7. The values shown in Table 3 were subtracted from the values shown in Table 6. The values shown in Table 5 were subtracted from the values shown in Table 4 to form Table 9. The values shown in Table 6 were subtracted from the values shown in Table 4 to form Table 10. The differences in the covariance matrices due to the different arrangements (reference period and period of record) of the basic observation data.

The basic data used in the computations are:

- (1) Table 4 employed wind data for the winter months (December, January, February) observed during the period Feb. 1950 thru Feb. 1955.
- (2) Table 5 employed wind data only for the month of January as observed from January 1951 December 1957.
- (3) Table 5 employed all wind date observed during the period January 1951 thru December 1957.

Therefore, the difference between Table 4 and Tables 5 and 6 result partially from combining the observational data on a monthly, seasonal, or annual basis. It may be seen from this presentation that a seasonal (winter) covariance matrix (Table 4) results in moderate conditions relative to the monthly (January) covariance matrix. Table 5 combines the upper air wind data for a winter month (January) only and, in general, has the highest values for the covariance matrix. Due to the influence of the summer months the annual covariance has the lower covariance values. This report, therefore, illustrates the relative differences in wind data statistically grouped according to different time reference periods. The selection of which covariance matrix to use depends upon the objective of the investigation and detail on wind input data desired.

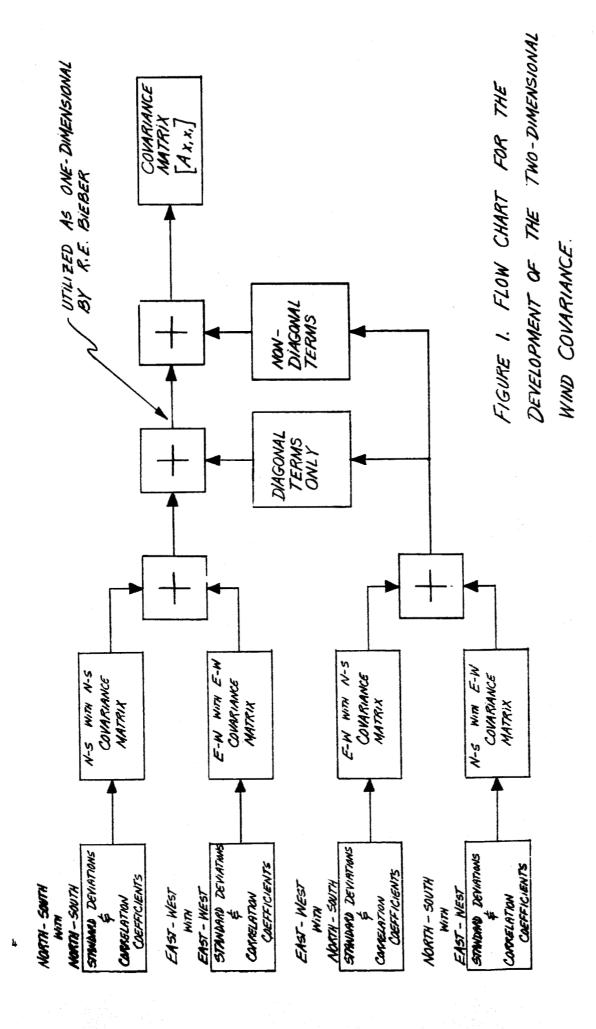
IV. UTILIZATION OF THE COVARIANCE MATRIX IN CONTROL AND TRAJECTORY STUDIES

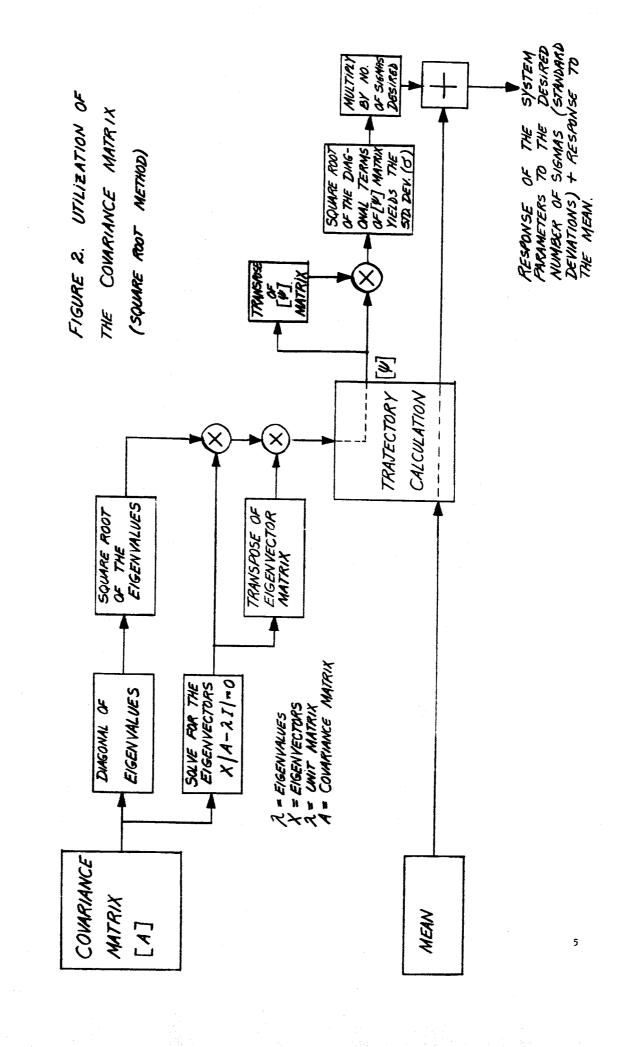
There are several ways in which the covariance matrix might be utilized in order to obtain a statistical description of the system response to winds and/or turbulence. The approach that seems to be the most efficient consists of taking the square root of the covariance matrix.

Figure 2 shows the flow of information when the square root of the covariance matrix method is used to develop a statistical description of the system parameters. Starting with the covariance matrix, the eigenvalues and eigenvectors are determined by using conventional techniques. For every eigenvalue there is a set of eigenvectors, consequently as the size of the covariance matrix increases the amount of work to solve for the eigenvalues and eigenvectors increases. The eigenvector matrix multiplied by the square root of the eigenvalue diagonal matrix is then multiplied by the transpose of the eigenvector matrix. The resultant matrix is the square root of the covariance matrix.

The columns for the square root of the covariance matrix are then fed into the computer program as discrete profiles. The response of the system parameters to each one of these discrete profiles represents a column of the (parameter response) matrix. When all of the profiles have been run by the computer the matrix can be completely assembled. This matrix is then multiplied by its transpose. The resulting matrix represents the response to the covariance matrix for all the system parameters. The square root of the diagonal terms of this matrix represents the standard deviation from the mean for each parameter as a function of altitude. The standard deviation from the mean is multiplied by the desired number of sigmas and then added to the response to the mean value for the winds. The resultant functions of altitude represent statistical description of the control system responses.

Structural bending is a function of the output parameters of the trajectory. Therefore, it is a straightforward matter to utilize these parameter values to determine actual structural loads.





Partico Part	TABLE (): INTERLEVEL AND INTRALEVEL CORRELATIONS BETWEEN WIND SPEED COMPONENTS WITH MEANS AND STANDARD DEVIATIONS OF WIND SPEED COMPONENTS BY ALTITUDE LEVELS	E.,		ZONAL AND MERIDIONAL WIND COMPONENT CORRELATIONS
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ş	-	11.40	13.21	.372	â	.63	7	8.	8	186	128	. 672	191	\$	989	. 636	3	. 878	. 585	926	*. 64	401 . 294	. 169	. 131	. 10	286.	. 039	.08			171	801.	1. 140.	149 .251
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•	2	21.32	21.79	907	\$23	<u>\$</u>	į	3	.743	. 192	5	. 964	. 679	16	. 923	. 949	203	. 189	34.	6. 999	. 186	478 . 349	19 . 208	. 134	. 110	. 105	. 078	160.	80	•	. 163	22.	. 021.	.170 .167
107	ž	19.71	20.56	14	220	426	. 579	. 671	.734	.781	. 83	. 846	. 859	910	689	. 913	946	. 11	. 608	3. 401.	. 623 . 515	15 .375	. 230	4	4 .116	91.3	.097	3		*	174	. 111	. 168	.241 .206
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Ĭ	*	. 5.78	13.16	621.	. 067	. 219	. 339	. 434	. 902	. 557	3	. 614	. 619	. 622	. 635	. 649	659	. 683	. 705	7. 121	367. 627.	193	111. 81	. 800	3		. 89	. 947	5	619	á	308	328	. 226 . 309
1390	z	. 5.61	14.19	61.	.082	. 226	ž	428	. 301	. 556	. 597	909	. 614	. 620	629	949	632	. 676 .	. 401	727 .7	728 .736	36 .765	191. 161	194	. 830	. 836	. 685	. 923	3	흵	3	; \$	379	\$15. 708
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2	62	- 5.52	16.81	951	. 083	. 235	. 34	. 428	. 508	. 578	. 626	. 649	.649	929	. 663	. 678	969	. 911.	. 141	7. 887.	217. 277.	787. 21	211. 112	194	. 833	. 834	1 . 872	906	.919	. 431		=======================================	6. 919.	. 902 . 449
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Ě	ä	- 9	21.03	. 143	.052	.237	38	4	. 538	386	645	. 678	. 678	.687	189	.708	111	. 745	. 164	1. 871.	. 769 . 742	111. 5	11 .763	. 800	. 425		. 839		ŧ	916	. 932	3	. 196.	.16
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STATION								-						
	STATION ELEVATION	LEVATION	STATION C	ON STATION ELEVATION STATION COORDINATES PERIOD OF OBSERVATION DATA SOURCE	PERI	PERIOD OF OBSERVATION	VATION	DATA 8	DATA SOURCE	•	PREPARED BY	D BY	PATR	PATRICK AFB, FLORIDA
Patrick AFB, Florida	7 matera MSL		28 deg 14 min	28 deg 14 min N, 80 deg 36 min W		Feb 1990 - Feb 1955	956	LMBD 4970	I.M.B.D 49703	Aerobe	Aeroballistics Laboratory Redatone Aranal, Alabama	ratory		
REFERENCE PERIOD Winter Months										16 May	1960		*	WINTER MONTHS
(Dec., Jan., Fab.) AR. (MSL) AB. Am.	٤	1 -	•		-	10	=	=	*	=	20	n	7	*
E S	26.43	28.92	28.04	29.46	30. 59	32.60	23.94	11.10	9.59	7.18	2.28	÷.	0.19	1, 53
N		95.85	83.09	89.96	98. 97	101.52	14.78	72.32	11.11	33.08	9.5	3. 38	17.93	19.36
•			150,28	140.14	155. 59	165.13	145.45	124. 65	71.01	61.54	26.35	13.36	21.57	31.14
				268.75 2	228. 63	244. 58	243.36	184. 41	139.56	90.28	34.01	7.7	21.08	40.93
•	•				424. 57	382. 52	320.77	259.67	197.69	129.71	8. 24	17.	ř.	52. 57
0.						683.25	433. 45	340.62	236.10	198.91	57.65	# #	¥.4	\$. #
71							783.90	407.03	283. 80	179.81	£. 4	40.15	31.32	56. 39
								608.63	281.27	119.11	59.41	25.01	29. 53	38. 42
•									376.23	165.92	80.21	#. 8	35.73	38. 67
•										260.21	80.28	31.85	# 7	49. 25
92											162.06	60.14	#.#	63. 62
a												143.89	7. 2.	77.67
*													166.98	117.37
92														195, 37
Ait. (MSL.)	J.	-	-	٥	-	10	2	=	91	=	20	23	7.7	26

																		П
COVARIANCE	PATRICK AFB, FLORIDA	JANUARY																
8	PATRIC		*	9. tt	1.01	2	7	18.90	10.04	3.33	13. 41	14.20	3.	39. 53	46.36	70.22	133.62	7
	enc,		72	3.	2	2	7.9	4-91	H	5.36	0.19	20. 15	39· (33. 66	3.6	109, 31		ř
(meters/sec) ²	PREPARED BY	aboratory 11. Alabama	n	4.67	£ .	2.17	 •	1.92	2.	7.90	17.50	33.95	33. 31	46.23	94,65			77
1	PREPA my Ballistics	Aerobalistics Laboratory Redstone Areezsi, Alabama 16 May 1960	20	3.13	1.	13,38	16.52	18.41	38.34	39.10	47.18	53.04	43.55	89.92				20
H OF JANU	Center		=	3.6	16.93	36.97	49.08	63.91	83.93	101.59	92.74	94.51	143.54					=
THE MONT	DATA SOURCE 1 Weather Records	r Bureau rth Carolina	2	6.08	39.42	77.43	106.16	137.57	170.05	213.38	193.73	283.17						91
ELOCITY AT INDICATED ALTITUDES AT PATRICK AFB FOR THE MONTH OF JANUARY	DATA National West	U. 6. Weather Bureau Asheville, North Carelina	2	15.39	3	120.28	176.30	246.09	314.09	384, 84	508. 61							7.
S AT PATRI	VATION 1987		=	20. 54	87.55	158.07	231.72	316.14	427.49	745. 25								12
ALTITUDE	PERIOD OF OBSERVATION Jan 1951 - Dec 1957		10	29.02	104, 15	174.74	253, 15	382, 64	683.68									10
INDICATED	PERIO 340			30.16	104. 51	167.98	245.45	403.99						•				8
LOCITY AT	STATION COORDINATES	•	•	30.21	104.74	156.87	283.98							*				•
T WIND V	STATION COC		-	24.63	96. 79	149.41												
RESULTAN	10N 8T		-	28.97	98.61													~
V GOVARIANCE OF RESULTANT WIND V	STATION ELEVATION		əje	23.60														»fc
4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4	NC	PERIOD																
	STATION	REFERENCE PERIOD	Alt. (MSL)	E 31	~	•	٠		91	21	2	91	•	92	22	7	92	Ait. (MSL.)

7	Table &6: Covariance of Resultant wind velocity at indicated altitudes at patrick afb for the annual	E OF RE	ULTANT W	IND VELOCIT	Y AT IND	CATED ALT	Trubes A:	F PATRICK	AFB FOR TI	IE ANNUA!		(meters/sec) ²		COVARIANCE
STATION	STATION ELEYATION	1	STATION COC	STATION COORDINATES		PERIOD OF OBSERVATION	VATION	Υď	DATA BOURCE		PRE	PREPARED BY		PATRICK AFB, FLORIDA
REFERENCE PERIOD						1047 3 907 - 1047 1090		U. S. West Ashaville,	U. S. Westher Bureau Ashaville, North Carolina		Aeroballistics Laberstory Redstone Aressah Alabama 16 May 1960	Laberador mah Alaba		* * * * * * * * * * * * * * * * * * *
Annual		_			_									WANDAL
Alk. (MSL) Alk. km (MSL) km	. sje	2	•	•	•	10	12	2	±	=	8	a	3	2
s fc	27.13	24, 49	22.98	22. 84	22.08	20.89	15.70	12. 30	10.11	7.27	9.84	3.0	. 4	\$
~		81.18	69.74	18.91	90.36	85. 67	35 . 28	70.69	83.09	38.78	18, 20		16.88	11.21
+			124. 49	127. 45 1	143.13	163.27	167.26	147.18	110.39	75.10	43.66	36. 33	ą. 2	3 3
•				218.21 2	215.75	249.48	262.77	232. 36	169.87	113.98	\$.	27.23	79.01	8. 18
6				•	342, 33	351.29	371.26	323. 60	232. 31	155.39	76. 97	27.38	*	1B. 44
01						577.35	510.69	433, 25	299. 68	200. 36	128.89	114.76	**	9.161
21							753.78	526.96	361.15	236.29	14.4	135.80	14.8	194.40
*								647.82	356.92	136.45	183.71	137.46	180.85	187.46
ž									362. 53	201. 51	134.13	117.69	126.97	186. 89
**										194.85	108.82	94. 19	103.45	375
02											114.14	63. 80	9.13	104. 55
27												109.08	:	111.69
72													137.54	136.53
79														189, 45
Alt. (MSL)	afe	7	$ \cdot $	۰	-	10	12	ž	91	=	92	77	77	26

		TABLE	TABLE #7: COMPARISON OF TABLE # 1 WITH TABLE #2	OF TABLE	1 WITH TABI	. E #2										
T ck	STATION Patrick AFB, Florida		STATION ELEVATION 7 meters MSL	STATION CO	STATION COORDINATES deg 14 min N, 80 deg 36 min	6 min W	The values shown in Table 2 were subtracted from the values shown in Table 1	hown in subtracted				Army Balli Aeroballas Redstone A 16 May 196	PREPARED BY Army Ballistics Missis Agency Aerobalistics Laboratory 16 May 1960	3Y de Agency lory lberna.	PATE	PATRICK AFB, FLORIDA
17	Altitude (MSL) km	IL) km	oj#	2	•	•		10	=	=	91	=.	22	77	z	97
	Z /	Meridional Mean m/e	1.381	-0.808	-0.804	-0.058	0.811	1, 309	1.723	1.343	0.190	0.570	0.331	-0.294	. 970	-0. 148
Altifude (MSL) km	Mean Si		0.234	-0.413	-0. 524	-0.264	0.055	0.406	1. 430	2, 280	1.777	0. 853	0.970	0.205	0.829	0.045
ų,	90	0, 105	610.0	0.011	0.007	0.031	0.004	0.067	9.108	0.113	0.173	0.167	0.087	0.120	0.022	-0.106
~	-0.209	-0.299	-0.007	0,069	-0.055	-0.058	-0.046	0.024	0.060	0.049	0.043	0.0	-0.074	0.026	0.038	-0.241
	-0.108	-0.334	-0,020	-0.028	6.079	-0.022	-0.038	0.017	0.035	9.040	0.068	0.118	0.008	0.050	-0.020	-0, 122
•	0.380	-0. 539	-0,053	-0. 027	-0.040	0.024	-0.042	0.022	0.105	0.083	0.092	0.163	-0.006	0.029	-0. 1 4	-0.113
	1.057	-0.162	-0.018	0.039	-0.001	-0.010	0.070	0.057	9.078	0.045	0.141	0, 181	0.127	-0.001	-0.138	-0.048
9	2. 414	-0.306	-0.022	-0.001	-0.025	-0.017	-0.047	-0.00	0.022	0.033	0.114	0.118	0.031	0.043	-0.204	-0.003
71	3. 853	0.182	-0.074	-0.040	-0.121	-0.103	-0.099	-0.067	-0.056	-0.041	9.078	0.081	0.023	-0.027	-0.146	0.047
	3. 813	1.692	-0.054	-0.029	-0.071	-0.101	-0116	-0.090	-0.014	-0, 121	0.060	0.117	-0.024	-0.062	-0.128	D. 048
91	2.547	2. 541	0.019	0.099	0.013	0.035	9.0	0.045	-0.003	0.014	-0.134	0.018	-0.025	-0.123	-0.238	-0,130
=	2. 997	4.334	0, 113	0.077	0,073	0.117	0.161	0.148	0.126	0.117	0,062	-0.023	-0.076	-0.121	-0.243	-0.113
2	-0. 452	3, 133	0,123	0.119	0.106	0.117	0.123	0.046	0.021	-0.061	-0.068	9.004	-0.044	-0.084	-0.174	-0.149
2	0.928	2.391	0.107	0.159	0.158	0.187	0.139	0.209	0.163	0.025	0.019	-0.106	-0.150	-0.018	-0. 326	-0.127
*	1. 669	3.595	0,167	0, 319	0.247	0,308	0.263	0.294	0.244	0.193	0.098	-0.00	-0.023	-0.076	0.082	-0.164
97	2.076	3. 646	0.265	0.318	0.315	0.319	0.230	0.230	0.252	0.060	0.140	-0.014	0.015	0.023	-0.068	-0.213

	٧g																		
	Patrick afb, florida		36	0.263	1.438	-0.121	-0.084	0.039	0,060	0, 132	0.128	0.046	0.062	-6. 102	-0.050	-0.013	-0.161	-0.084	0.029
	PATRI		ä	0.130	1.199	0.620	0.049	-0.037	9.0	-0.114	. is	9.09	9.9	6 . 141	6. 14	908 '9	9.15	- 188	-6.177
	Agency 7	1	22	0.106	-0.028	-0.088	-6.078	6.691	0.063	980.0-	0.0	0.019	0.00	0.03	0. 65s	6.004	-0.076	-0.24	-0.256
	PREPARED BY Histics Missile Stics Laborator		92	0.161	1.090	0.082	0.061	0. 128	0.117	0.138	0.110	0.091	0.083	40.0	0.008	0.173	-0.367	.6. XE	-0.347
	PREPARED BY Army Ballistics Missils Agency Asroballistics Laborates	16 May 1960		0.610	2, 109	0.088	0.073	0.105	0, 167	0.138	0. 101	0.094	0.133	0.098	0.103	-0.343	-0. 521	9.	-0.485
			16	1.360	2.987	.0. 161	0,051	0.073	0.011	0.079	0,035	0.054	0,065	0,071	-0, 255	-0.371	-0, 456	-0. 470	-0. 497
			14	2.113	2. 640	0.168	0.039	0.065	0,054	0.028	-0.010	6.083	0,060	6.181	-0.294	-0.486	-0.561	-0.501	-0. 563
	,		12	1,603	3.220	6.147	0.051	6.072	B. 069	0.022	9.03	0.128	6.173	-0.196	-0.279	6.481	-0.482	9.44	-0. 450
	own in subtracted		2	0.729	3. 826	9, 161	9.0	9.09	0, 031	0.026	9.13	-6.155	6.19	ė.	0.298	è.	-0.408	. 360	-0.416
	o The values shown in Table 3 were subtracted from the values shown is Table 1		-	0.171	3,305	0.123	0.029	9.0	0,010	0. 167	6.04	-0. 191	-0. 220	-0.209	97.0	90 .0	99 '0	-0.396	-0. 390
	*		•	-0.538	2. 666	0.109	0.013	0.021	0.077	-0, 074	-0.108	0.215	-0.221	-0.230	-0. 332	-0.392	-0.393	-0.361	-0. 320
	COORDINATES N, 40 deg 36 min W		•	-1.184	1,666	0.086	0.003	0.032	-0.062	-0.057	-0,083	-0.170	-0.142	-0.186	-0.262	-0.294	-0.314	-0. 220	-0. 200
H TABLE #3	FTATION CO		2	-1. 638	1.367	0.058	-0.093	-0.023	-0.009	. 0. 032	0.031	-0.00	-0.001	0.003	-0.141	-0,181	-0.204	-0.036	-0.016
BLE #1 WIT			ofe	0.811	0.414	-0.116	-0.051	0.007	0.023	0.039	0.065	0.034	0.041	0.029	-0.150	-0.078	-0.10	-0.14	-0.053
Table #8: Comparison of table #1 with table	STATION ELEVATION 7 meters MSL				- /										71.00				
OMPARI			8L) km	Meridional Mess m/		-0.055	0.341	-0.234	-0.889	-1.272	-2, 336	-3. 698	-3. 618	-2. 379	0. 574	0,933	1.31	-0.965	-0. 444
BLE SE C	STATION Patrick AFB, Florida		Altitude (MSL) km	×/.	Mean Mean	0.994	3.011	5. 822	8. 830	11.907	15.144	17.303	17.613	15, 527	12.767	6, 628	9.018	11.269	13, 656
٤	Patrick				(MSL) km	y g	~	*	•	•	9	22	:	91	:	07	77	77	36

All: All: All: All: All: All: All: All:		##ATION CO	28 deg 14 mis N, 80 deg 36 mis W 8.06 6.58 8 13.35 14.04 33. 29.79 33.21 12.		- 1 d	9. 34 12 13 9. 35	=		Army Aerob Redet	PREPARED BY Army Ballistics Missile Agency Aeroballistics Laboratory	PREPARED BY Army Ballistics Missils Agency Asroballistics Laboratory Redistors Arsesal, Alabama 16 May 1960	Ž.	PATRICK AFB, FLORIDA
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o ·	* \$ 57	4 40 41 44 44 44 44 44 44 44 44 44 44 44 44		-		5. 34 9. 35	3		-	y 1960			
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· · · · · · · · · · · · · · · · · · ·		4		* *			5	3	- 2.70	. 8.70	- 11. 39	1.08	. 1. 5
• • a a a a a				:		- 21.61	- 23.54	- 15. 32	- 13,56	- 17.31	23.03	- 20.45	21.04
• <u>•</u> <u>•</u> <u>•</u> <u>•</u> •			•		i j	- 19.41	-100.70	. 30. 31	- 23,70	- 35.83	- 40.88	4.4	3.
2 2 2 2			•	81.24	37.23	- 90. 4	- 63.93	3, 12, 63	- 25.68	- 46, 55	- 69.90	- 70. £	- 10.01
g 5 9 1					105.90	- 77.24	- 92.63	- 63.58	. 4. 5	1 68.34	- 68.44	. 66.83	- 97.52
* * *						30.12	-119, 93	- 77.38	- 36, 48	- 87.93	. 98. 38	-117.84	-133,01
. 2 1							. 39, 19	- 75, 65	- 57.33	. 94.30	-112.67	-121.06	-152,04
								13.70	- 35.59	- 53, 92	- 69.89	- 91.24	-117.22
_									65,36	- 28.54	. 56.30	- 59.16	- 75, 37
8										47.92	- 23.66	- 31.89	. 36. 33
27											34, 81	- 19.04	- 34.02
**												21.4	13.16
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AIE. (MBL)	~	-	,		2	=	=	2	18	20	22	ž	36

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